

# HOW TO RUN AN EXAMPLE OF COUPLING BETWEEN FDS AND SAFIR

## 1. SPECIFIC FILES YOU NEED TO RUN AN FDS-SAFIR ANALYSIS

- The **modified executable of FDS (FDS\_SAFIR.exe)** able to produce the transfer file (i.e. the file that contains temperatures and intensities calculated by FDS). This executable of FDS differs from the “official” one downloadable from the website <http://www.fire.nist.gov/fds/>.
- A **2012 version (or later) of SAFIR (either SAFIR2012\_32.exe for 32bit OS or SAFIR2012\_64.exe for 64bit OS)** that includes all routines necessary to perform thermal analyses on the basis of FDS data.

## 2. EXAMPLE

### A) COMPARTMENT MODELLED IN FDS

#### GEOMETRY

The compartment  $6 \times 6 \times 3 \text{ m}^3$ : The floor, the ceiling and one perimetral wall are modelled whereas the others 3 walls are openings.

#### MATERIALS

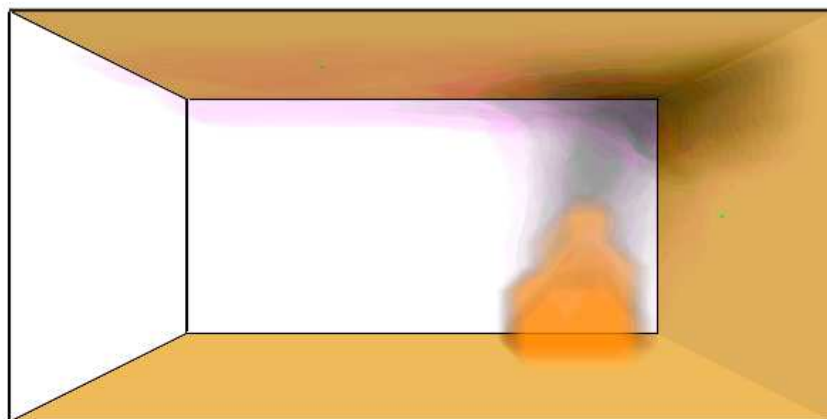
The floor, ceiling and wall are made of concrete whose thermal material properties are derived from the EN1992-1-2.

#### LOCALISED FIRE

A localised fire  $1 \times 1 \text{ m}^2$  with constant  $\text{HRR} = 1000 \text{ kW/m}^2$  is located at  $x = 4.5 \text{ m}$ ,  $y = 3 \text{ m}$  and  $z = 0 \text{ m}$ .

**NOTE:** that in the following figure no structural elements across the compartment is modelled in FDS.

Smokeyview 5.6 – Oct 29 2010



Frame: 267

Time: 168.9

>80 (kW/m<sup>3</sup>)

## B) STRUCTURE MODELLED IN SAFIR

### GEOMETRY

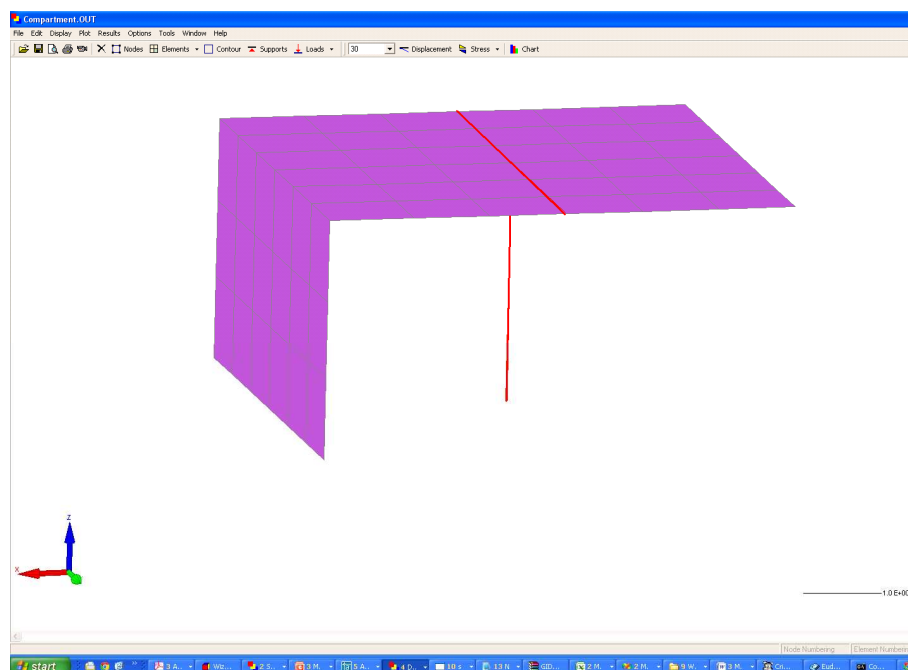
The ceiling and the wall are also modelled in SAFIR by means of shell elements. The ceiling and the wall differ from the thickness (150 mm for the ceiling and 200 mm for the wall). Thus, they are two shell element types.

Moreover, a composite beam made of a HE400B profile and a concrete slab of 150 mm, as well as a column made of a steel tube (diameter 300 mm and thickness 10 mm), are modelled with beam elements.

### MATERIALS

The slab, and wall are made of concrete whose thermal and mechanical material properties are derived from the EN1992-1-2 and EN1992-1-1, respectively.

The beam and the tube are made of steel the thermal and mechanical material properties of which are derived from the EN1993-1-2.



## 3. HOW TO RUN FDS AND CREATE THE TRANSFER FILE

- The executable FDS\_SAFIR.exe provided to you in the folder FDS\_Files has to be in the same folder as the input file .fds used to simulate the scenario in FDS.
- The input file of FDS .fds can be written in a text editor following the standard syntax of FDS. However, as this executable of FDS differs from the official one, additional commands have to be written in order to ask FDS to create the transfer file as an output. Basically, there are two commands specifically conceived for this purpose and implemented in the modified version of FDS:

```
-----  
&HEAD CHID='Localised_Fire', TITLE='Localised_Fire' /
```

```
&MESH XB=0.0,6.0,0.0,6.0,0.0,3.0, IJK =24,24,12 /
```

```
&RADI NUMBER_RADIATION_ANGLES=64 /
```

&MISC NOISE=.FALSE. /

&FDStoSAFIR STATUS=.TRUE.,T\_BEGIN=1., T\_END=601. DT=30.,  
XB=0.0,6.0,0.0,6.0,0.0,3.0, ORIENTATION=-1,1,-2,2,-3,3 /

&PointtoSAFIR XYZ= 4.5 3.0 2.80 /

&TIME T\_END=601. DT=5.0 /

-----CONCRETE CEILING-----

&MATL ID = 'concrete'  
EMISSION = 0.7  
DENSITY = 2300.  
CONDUCTIVITY\_RAMP = 'k\_ramp'  
SPECIFIC\_HEAT\_RAMP = 'c\_ramp' /

-----SILICEOUS CONCRETE AND UPPER LIMIT FOR CONDUCTIVITY EN1992-1-2-----

&RAMP ID='k\_ramp', T=20., F=1.9514 /  
&RAMP ID='k\_ramp', T=100., F=1.7656 /  
&RAMP ID='k\_ramp', T=200., F=1.5526 /  
&RAMP ID='k\_ramp', T=300., F=1.3610 /  
&RAMP ID='k\_ramp', T=400., F=1.1908 /  
&RAMP ID='k\_ramp', T=500., F=1.0420 /  
&RAMP ID='k\_ramp', T=600., F=0.9146 /  
&RAMP ID='k\_ramp', T=700., F=0.8086 /  
&RAMP ID='k\_ramp', T=800., F=0.7240 /  
&RAMP ID='k\_ramp', T=900., F=0.6608 /  
&RAMP ID='k\_ramp', T=1000., F=0.6190 /  
&RAMP ID='k\_ramp', T=1100., F=0.5986 /  
&RAMP ID='k\_ramp', T=1200., F=0.5996 /

-----3% MOISTURE CONTENT EN1992-1-2-----

&RAMP ID='c\_ramp', T=20., F=0.900 /  
&RAMP ID='c\_ramp', T=100., F=0.900 /  
&RAMP ID='c\_ramp', T=115., F=2.020 /  
&RAMP ID='c\_ramp', T=200., F=1.000 /  
&RAMP ID='c\_ramp', T=400., F=1.100 /  
&RAMP ID='c\_ramp', T=1200., F=1.100 /

-----SURF ID-----

&SURF ID = 'ceil\_floor'  
MATL\_ID = 'concrete'  
THICKNESS = 0.15 /

&SURF ID = 'wall'  
MATL\_ID = 'concrete'  
THICKNESS = 0.20 /

----- WALLS -----

&OBST XB=6.0,6.0,0.0,6.0,0.0,3.0,SURF\_ID='wall' /  
&OBST XB=0.0,6.0,0.0,6.0,0.0,0.0,SURF\_ID='ceil\_floor' /  
&OBST XB=0.0,6.0,0.0,6.0,3.0,3.0,SURF\_ID='ceil\_floor' /

```

&VENT MB='XMIN',SURF_ID='OPEN' /
&VENT MB='YMIN',SURF_ID='OPEN' /
&VENT MB='YMAX',SURF_ID='OPEN' /

-----SQUARE FIRE-----

&SURF ID = 'fire'
      HRRPUA = 2000.0 /

&VENT XB=4.0,5.0,2.5,3.5,0.0,0.0, SURF_ID='fire'

&DEVC XYZ=2.0,3.0,3.0, QUANTITY='WALL TEMPERATURE', IOR=-3, ID='wall'
/
&DEVC XYZ=6.0,3.0,1.5, QUANTITY='WALL TEMPERATURE', IOR=-1, ID='wall'
/

&TAIL /

```

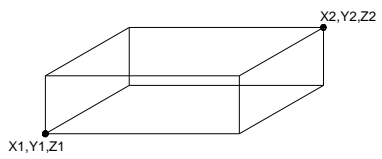
#### 1) FDStoSAFIR:

it allows recording at the centre of each cell of the compartment (or a subdomain of it) modelled in FDS temperature, convection coefficient and radiant intensities. In the given example

```

&FDStoSAFIR STATUS=.TRUE.,T_BEGIN=1., T_END=601. DT=30.,
XB=0.0,6.0,0.0,6.0,0.0,3.0, ORIENTATION=-1,1,-2,2,-3,3 /

```

COMMAND	DEFINITION	
STATUS	ACTIVATION OF THE INTERFACE	DEFAULT VALUE .FALSE.
T_BEGIN	TIME AT WHICH THE WRITING OF DATA IN THE TRANSFER FILE STARTS [s]	-
T_END	TIME AT WHICH THE WRITING OF DATA IN THE TRANSFER FILE FINISHES [s]	-
DT	TIME STEP OF THE WRITING OF DATA IN THE TRANSFER FILE [s]	-
XB	DIMENSIONS OF THE DOMAIN WHERE TO RECORD DATA	X1,X2,Y1,Y2,Z1,Z2 6 VALUES IN m 
ORIENTATION	IF THE FLUX IS REQUIRED IN SOME POINT OF THE DOMAIN BY MEANS OF THE PointtoSAFIR COMMAND, IT GIVES THE ORIENTATION OF THE NORMAL TO SURFACE OF THE RECORDED FLUXES	-1,1,-2,2,-3,3 6 DIRECTIONS  (1 IS PARALLEL TO THE x-AXIS, 2 TO y-AXIS AND 3 TO THE z-AXIS)

## 2) PointtoSAFIR

it allows recording at one point of the compartment modelled in FDS temperature, convection coefficient and fluxes whose normal to surface has orientation according to what specified in ORIENTATION in the FDStoSAFIR command.

An example of syntax

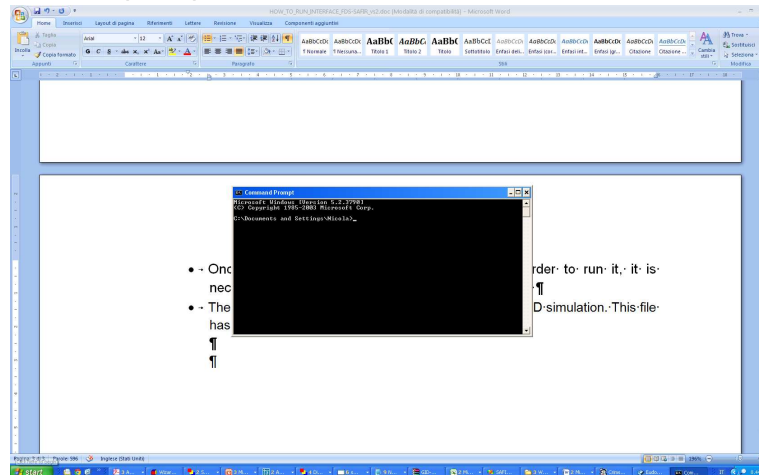
```
&PointtoSAFIR XYZ= 4.5 3.0 2.80 /
```

COMMAND	DEFINITION	
XYZ	COORDINATES OF THE POINT	<p>X,Y,Z 3 VALUES IN m</p> <p>On the basis of the example given previously for FDStoSAFIR, the transfer file will contain temperature, convection coefficient and flux of normal parallel to the x-axis and pointing toward -x of the centre of cell where the point of coordinates XYZ= 4.5 3.0 2.80 is contained.</p>

- The number of radiant intensity to be written in the transfer file is given by the standard FDS command `RADI NUMBER_RADIATION_ANGLES`. The following table provides the number to be assigned to the `NUMBER_RADIATION_ANGLES` in order to get a certain number of radiant intensities in transfer file.

NUMBER_RADIATION_ANGLES	RESULTING NUMBER OF INTENSITIES
12	16
24	24
30	32
36	40
48	48
52	56
56	64
64	72
80	80
86	88
90	96
100	104

- Once the .fds input file for FDS is written, in order to run it, it is necessary to open a Command prompt window



and to go in folder where the executable FDS\_SAFIR.exe is located along with the .fds input file. Then, type `fds_safir name_input_file.fds` and FDS will start to run.

- Once the FDS simulation is finished check with SMOKEVIEW the results of the simulation. Double click on the .smv file created in the same folder.
- Finally, the **transfer file** has been produced in the same folder where the executable and the input file of FDS are located. This file has extension .Fts and it has to be renamed to `cfd_trilin.txt` in order to be successfully used as input for the SAFIR thermal analyses.

#### 4. HOW TO RUN A THERMAL ANALYSIS IN SAFIR WITH DATA PROVIDED BY FDS

- The procedure follows the same steps needed to run in SAFIR a scenario of a localised fire by employing the Hasemi model.
- The `cfd_trilin.txt` file must be located in the same folder where the thermal input file is located.

##### A) WRITE THE MECHANICAL INPUT FILE

- The first step is write the input file (in this example `Compartment.in`) needed to run the mechanical analysis (it is a `Safir_Structural_3D` problem type). It will be used in the thermal analysis in order to identify the position of the structural points in the compartment.

Note that two types of beam elements and two types of shell elements are included in the present example.

Moreover, all structural elements at the boundaries (slab and wall in particular) are located in correspondence to their centreline axes, which means that they surely outside the CFD domain. Also the nodeline of the composite beam is at the level of the slab centreline.

The mechanical input file must be located in the same folder where the thermal input file is located.

-----  
LOCALISED FIRE - MECHANICAL FILE

```

      NNODE      84
      NDIM       3
      NDDLMAX    7
EVERY_NODE      0
      FROM 1 TO 42 STEP    1 NDDL    6
      FROM 43 TO 49 STEP    1 NDDL    7
      FROM 50 TO 70 STEP    1 NDDL    6
      FROM 71 TO 73 STEP    1 NDDL    7
      FROM 74 TO 82 STEP    1 NDDL    1
      FROM 83 TO 84 STEP    1 NDDL    0
END_NDDL
      STATIC      PURE_NR
      NLOAD       1
      OBLIQUE     0
      COMEBACK    1.0e-5
RENUMGEO 1
      NMAT        4
ELEMENTS
      BEAM      9      2
      NG 2
      NFIBER    414
      SHELL     54      2
      NGTHICK   3
      NGAREA    2
      NREBARS   2
END_ELEM
      NODES
      NODE      1      6.100    0.000   -0.075
      NODE      2      6.100    1.000   -0.075
      NODE      3      6.100    2.000   -0.075
      NODE      4      6.100    3.000   -0.075
      NODE      5      6.100    4.000   -0.075
      NODE      6      6.100    5.000   -0.075
      NODE      7      6.100    6.000   -0.075
      NODE      8      6.100    0.000    1.000
      NODE      9      6.100    1.000    1.000
      NODE     10      6.100    2.000    1.000
      NODE     11      6.100    3.000    1.000
      NODE     12      6.100    4.000    1.000
      NODE     13      6.100    5.000    1.000
      NODE     14      6.100    6.000    1.000
      NODE     15      6.100    0.000    2.000
      NODE     16      6.100    1.000    2.000
      NODE     17      6.100    2.000    2.000
      NODE     18      6.100    3.000    2.000
      NODE     19      6.100    4.000    2.000
      NODE     20      6.100    5.000    2.000
      NODE     21      6.100    6.000    2.000
      NODE     22      6.100    0.000    3.075
      NODE     23      6.100    1.000    3.075
      NODE     24      6.100    2.000    3.075
      NODE     25      6.100    3.000    3.075
      NODE     26      6.100    4.000    3.075
      NODE     27      6.100    5.000    3.075
      NODE     28      6.100    6.000    3.075
      NODE     29      5.000    0.000    3.075
      NODE     30      5.000    1.000    3.075
      NODE     31      5.000    2.000    3.075
      NODE     32      5.000    3.000    3.075
      NODE     33      5.000    4.000    3.075
      NODE     34      5.000    5.000    3.075
      NODE     35      5.000    6.000    3.075
      NODE     36      4.000    0.000    3.075
      NODE     37      4.000    1.000    3.075
      NODE     38      4.000    2.000    3.075
      NODE     39      4.000    3.000    3.075
      NODE     40      4.000    4.000    3.075
      NODE     41      4.000    5.000    3.075
      NODE     42      4.000    6.000    3.075
      NODE     43      3.000    0.000    3.075
      NODE     44      3.000    1.000    3.075

```

NODE	45	3.000	2.000	3.075				
NODE	46	3.000	3.000	3.075				
NODE	47	3.000	4.000	3.075				
NODE	48	3.000	5.000	3.075				
NODE	49	3.000	6.000	3.075				
NODE	50	2.000	0.000	3.075				
NODE	51	2.000	1.000	3.075				
NODE	52	2.000	2.000	3.075				
NODE	53	2.000	3.000	3.075				
NODE	54	2.000	4.000	3.075				
NODE	55	2.000	5.000	3.075				
NODE	56	2.000	6.000	3.075				
NODE	57	1.000	0.000	3.075				
NODE	58	1.000	1.000	3.075				
NODE	59	1.000	2.000	3.075				
NODE	60	1.000	3.000	3.075				
NODE	61	1.000	4.000	3.075				
NODE	62	1.000	5.000	3.075				
NODE	63	1.000	6.000	3.075				
NODE	64	0.000	0.000	3.075				
NODE	65	0.000	1.000	3.075				
NODE	66	0.000	2.000	3.075				
NODE	67	0.000	3.000	3.075				
NODE	68	0.000	4.000	3.075				
NODE	69	0.000	5.000	3.075				
NODE	70	0.000	6.000	3.075				
NODE	71	3.000	3.000	2.000				
NODE	72	3.000	3.000	1.000				
NODE	73	3.000	3.000	-0.075				
NODE	74	3.000	3.000	2.5375				
NODE	75	3.000	3.000	1.500				
NODE	76	3.000	3.000	0.500				
NODE	77	3.000	0.500	3.075				
NODE	78	3.000	1.500	3.075				
NODE	79	3.000	2.500	3.075				
NODE	80	3.000	3.500	3.075				
NODE	81	3.000	4.500	3.075				
NODE	82	3.000	5.500	3.075				
NODE	83	3.000	6.100	4.000				
NODE	84	3.100	3.000	-0.100				

FIXATIONS

BLOCK	1	F0	F0	F0	NO	NO	NO	NO
BLOCK	2	F0	NO	F0	NO	NO	NO	NO
BLOCK	3	F0	NO	F0	NO	NO	NO	NO
BLOCK	4	F0	NO	F0	NO	NO	NO	NO
BLOCK	5	F0	NO	F0	NO	NO	NO	NO
BLOCK	6	F0	NO	F0	NO	NO	NO	NO
BLOCK	7	F0	NO	F0	NO	NO	NO	NO
BLOCK	64	F0	F0	F0	NO	NO	NO	NO
BLOCK	65	F0	NO	F0	NO	NO	NO	NO
BLOCK	66	F0	NO	F0	NO	NO	NO	NO
BLOCK	67	F0	NO	F0	NO	NO	NO	NO
BLOCK	68	F0	NO	F0	NO	NO	NO	NO
BLOCK	69	F0	NO	F0	NO	NO	NO	NO
BLOCK	70	F0	NO	F0	NO	NO	NO	NO
BLOCK	73	F0	F0	F0	F0	F0	F0	F0

END\_FIX

NODOFBEAM

**beam1.tem**

TRANSLATE	1	1
TRANSLATE	2	3

END\_TRANS

**column.tem**

TRANSLATE	1	1
-----------	---	---

END\_TRANS

ELEM	1	43	77	44	83	1
ELEM	2	44	78	45	83	1
ELEM	3	45	79	46	83	1
ELEM	4	46	80	47	83	1
ELEM	5	47	81	48	83	1
ELEM	6	48	82	49	83	1
ELEM	7	46	74	71	84	2
ELEM	8	71	75	72	84	2
ELEM	9	72	76	73	84	2

NODOFSHELL

**wall.tsh**



```

TRANSLATE      1      2
TRANSLATE      2      4
END_TRANS
slab.tsh
TRANSLATE      1      2
TRANSLATE      2      4
END_TRANS
ELEM1          1          2          9          8      1
ELEM           2          2          3          10         9      1
ELEM           3          3          4          11         10     1
ELEM           4          4          5          12         11     1
ELEM           5          5          6          13         12     1
ELEM           6          6          7          14         13     1
ELEM           7          8          9          16         15     1
ELEM           8          9         10          17         16     1
ELEM           9         10         11          18         17     1
ELEM          10         11         12          19         18         1
ELEM          11         12         13         20         19         1
ELEM          12         13         14         21         20         1
ELEM          13         15         16         23         22         1
ELEM          14         16         17         24         23         1
ELEM          15         17         18         25         24         1
ELEM          16         18         19         26         25         1
ELEM          17         19         20         27         26         1
ELEM          18         20         21         28         27         1
ELEM          19         22         23         30         29         2
ELEM          20         23         24         31         30         2
ELEM          21         24         25         32         31         2
ELEM          22         25         26         33         32         2
ELEM          23         26         27         34         33         2
ELEM          24         27         28         35         34         2
ELEM          25         29         30         37         36         2
ELEM          26         30         31         38         37         2
ELEM          27         31         32         39         38         2
ELEM          28         32         33         40         39         2
ELEM          29         33         34         41         40         2
ELEM          30         34         35         42         41         2
ELEM          31         36         37         44         43         2
ELEM          32         37         38         45         44         2
ELEM          33         38         39         46         45         2
ELEM          34         39         40         47         46         2
ELEM          35         40         41         48         47         2
ELEM          36         41         42         49         48         2
ELEM          37         43         44         51         50         2
ELEM          38         44         45         52         51         2
ELEM          39         45         46         53         52         2
ELEM          40         46         47         54         53         2
ELEM          41         47         48         55         54         2
ELEM          42         48         49         56         55         2
ELEM          43         50         51         58         57         2
ELEM          44         51         52         59         58         2
ELEM          45         52         53         60         59         2
ELEM          46         53         54         61         60         2
ELEM          47         54         55         62         61         2
ELEM          48         55         56         63         62         2
ELEM          49         57         58         65         64         2
ELEM          50         58         59         66         65         2
ELEM          51         59         60         67         66         2
ELEM          52         60         61         68         67         2
ELEM          53         61         62         69         68         2
ELEM          54         62         63         70         69         2
PRECISION 1.0e-3
LOADS
FUNCTION      FLOAD
DISTRSH       19 0.000000 0.000000 -5310.000000
GDISTRSH      54 0.000000 0.000000 -5310.000000 1
END_LOAD
MATERIALS
STEELEC3EN
2.10e+11      3.00e-01      3.55e+08 1200.      0.
SILCONC2D
3.00e-01      3.00e+07      3.00e+06 0.
INSULATION
STEELEC2
2.06e+11      3.00e-01      5.00e+08 1200.      0.
TIME

```

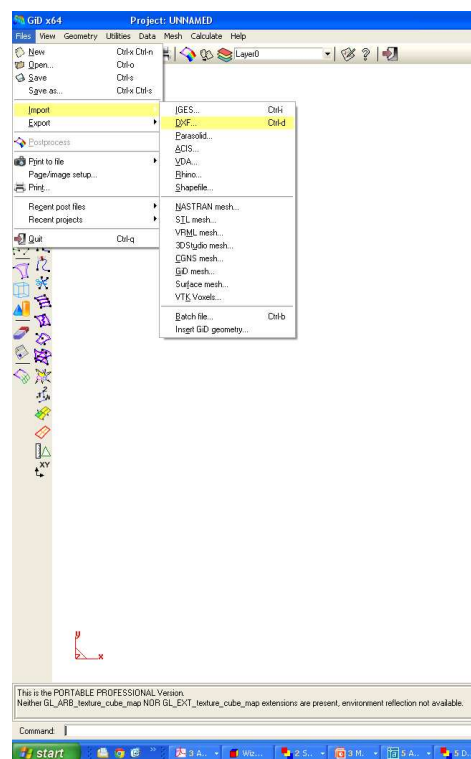
```

1.0      600.0
ENDTIME
EPSTH
IMPRESSION
TIMEPRINT
30.0     600.0
END_TIMEPR
PRINTREACT
PRINTMN
PRINTFHE
PRINTDEPL

```

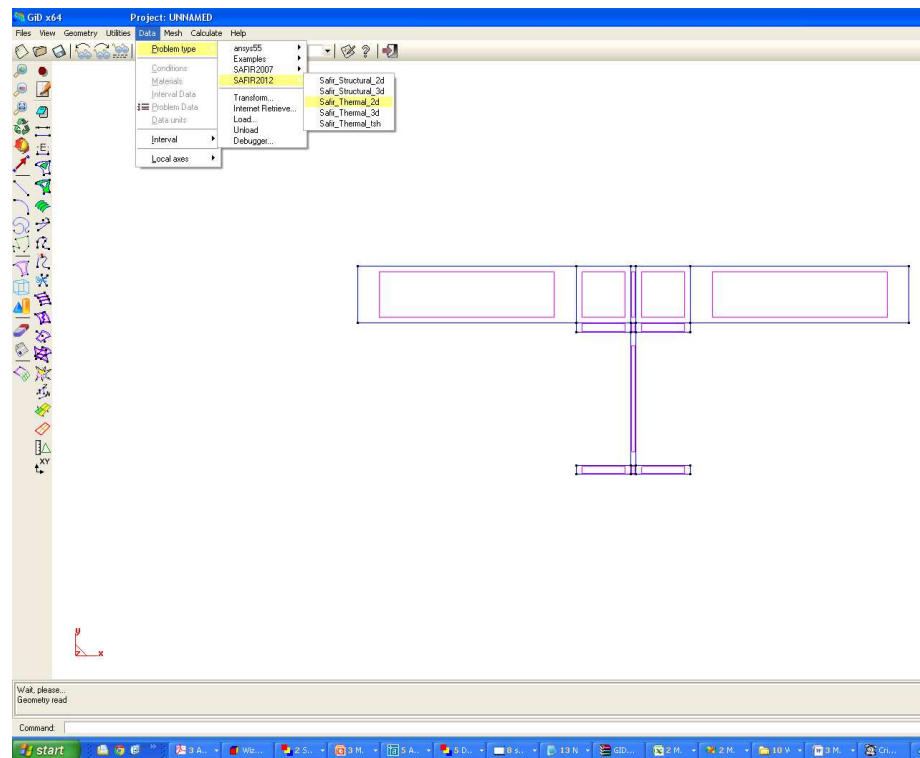
## B) CREATE THE THERMAL INPUT IN GiD FILES AND RUN THERMAL ANALYSIS

- If you use GiD new GiD - SAFIR interface files have been developed to include the option to run thermal analyses that exploit CFD data. In order to speed up the process .dxf files which contain the **section layout** of both beam elements are already provided to you in the folder DXF\_Files.

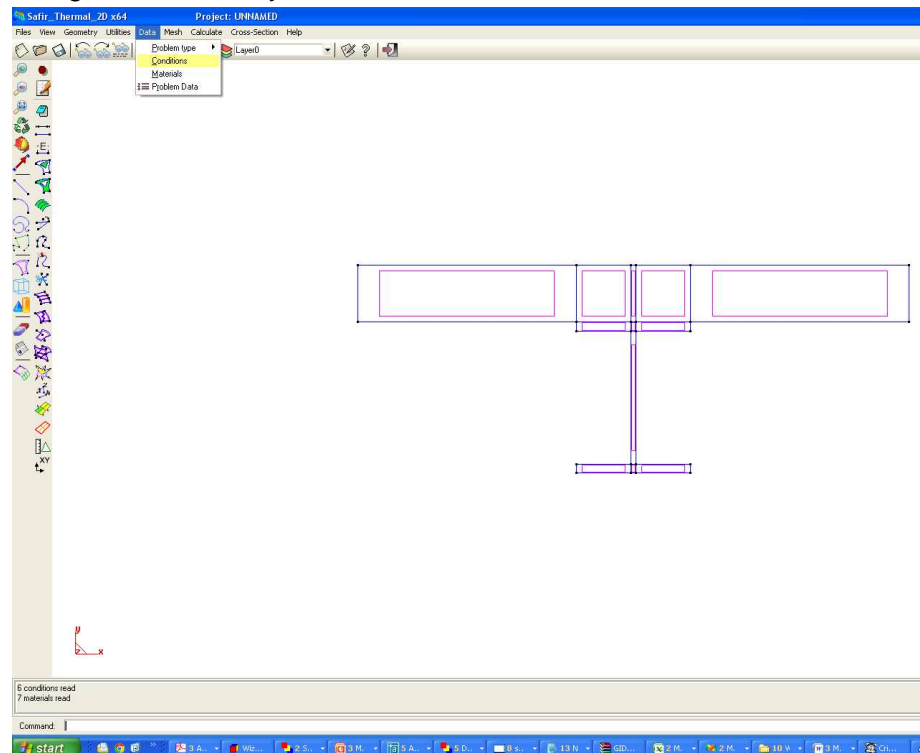


## COMPOSITE BEAM

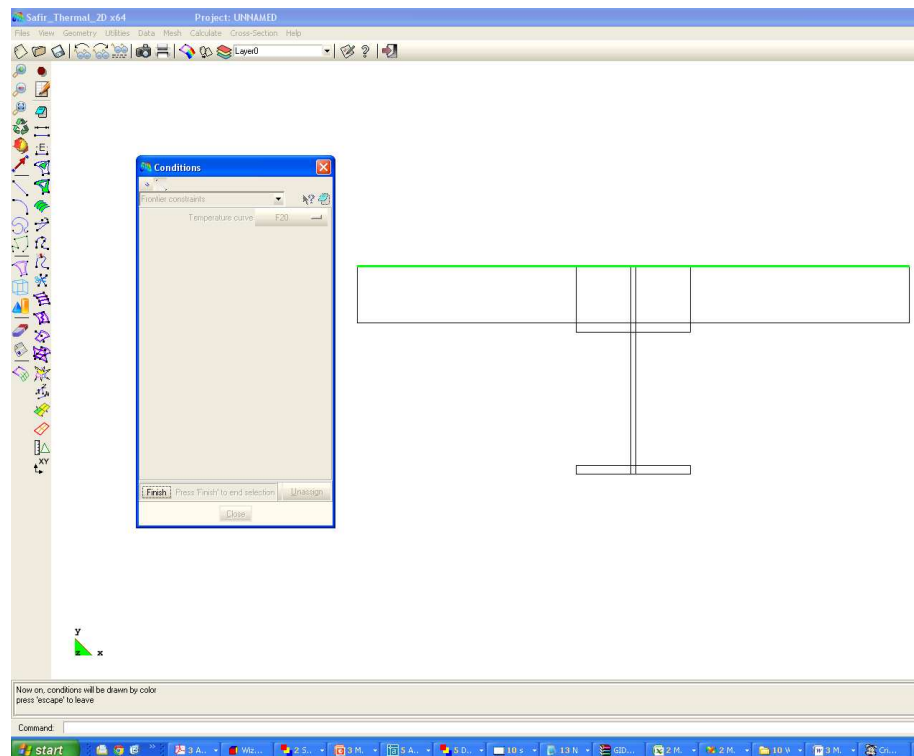
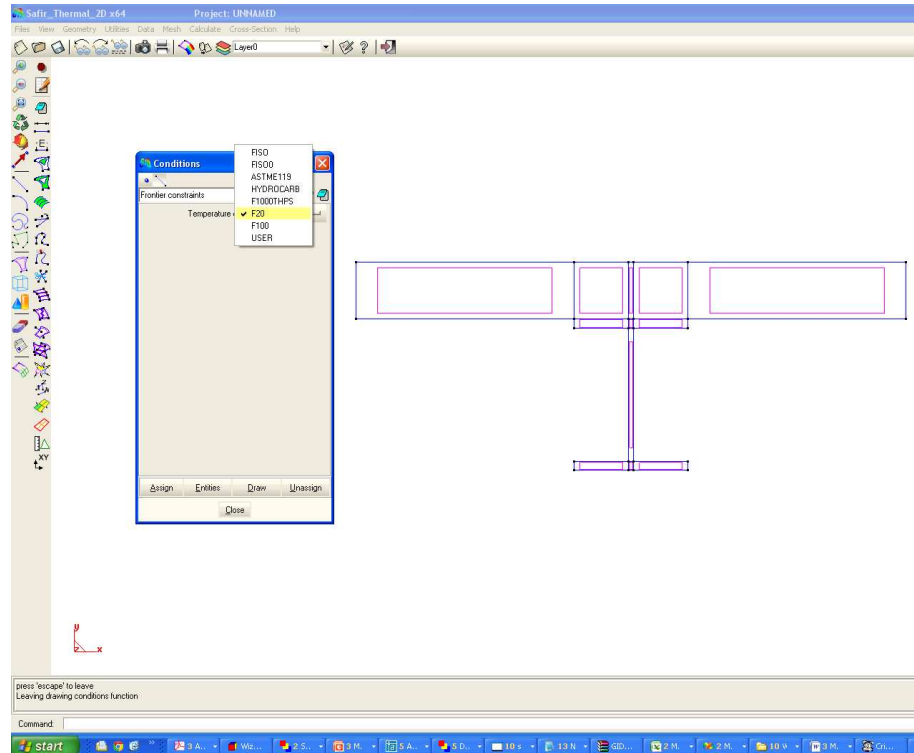
Select the **Problem type** -> Safir\_Thermal\_2D in the new SAFIR 2012 GiD - SAFIR interface



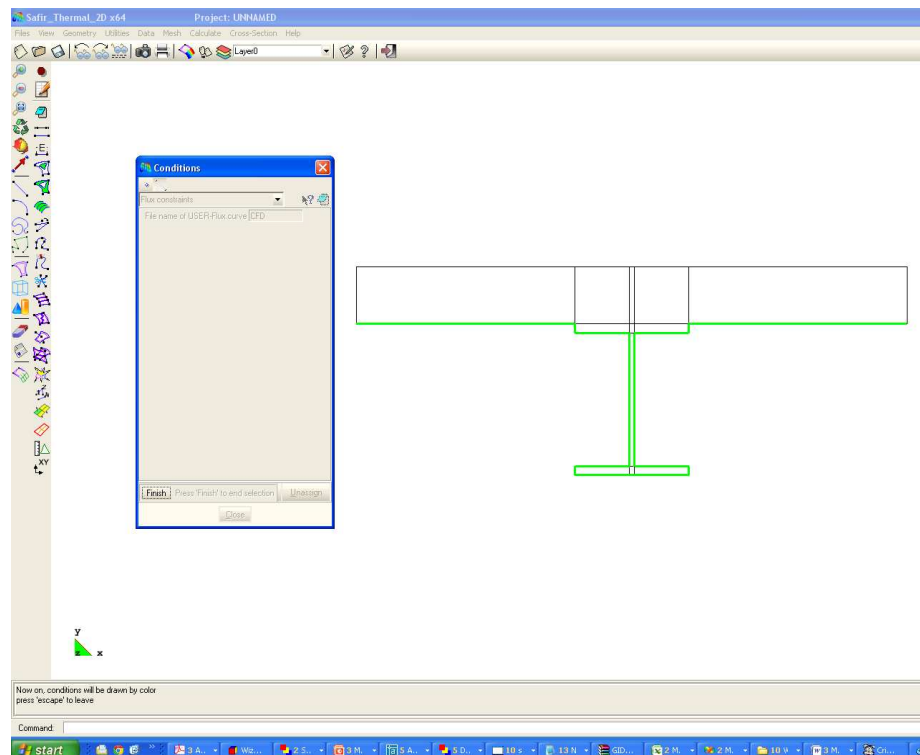
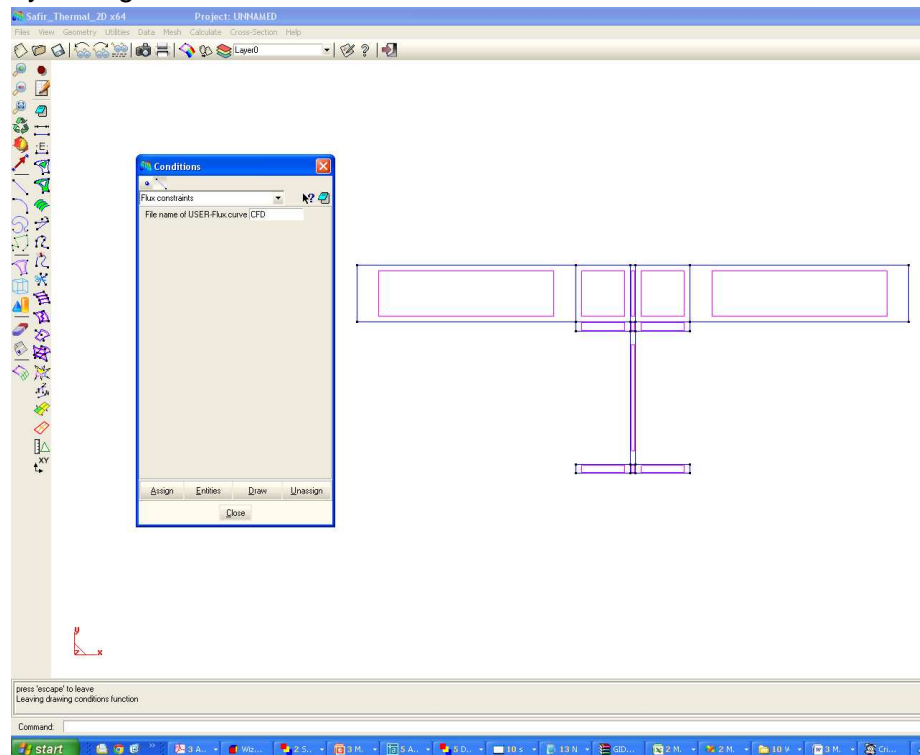
Assign the **Boundary Conditions** to the section



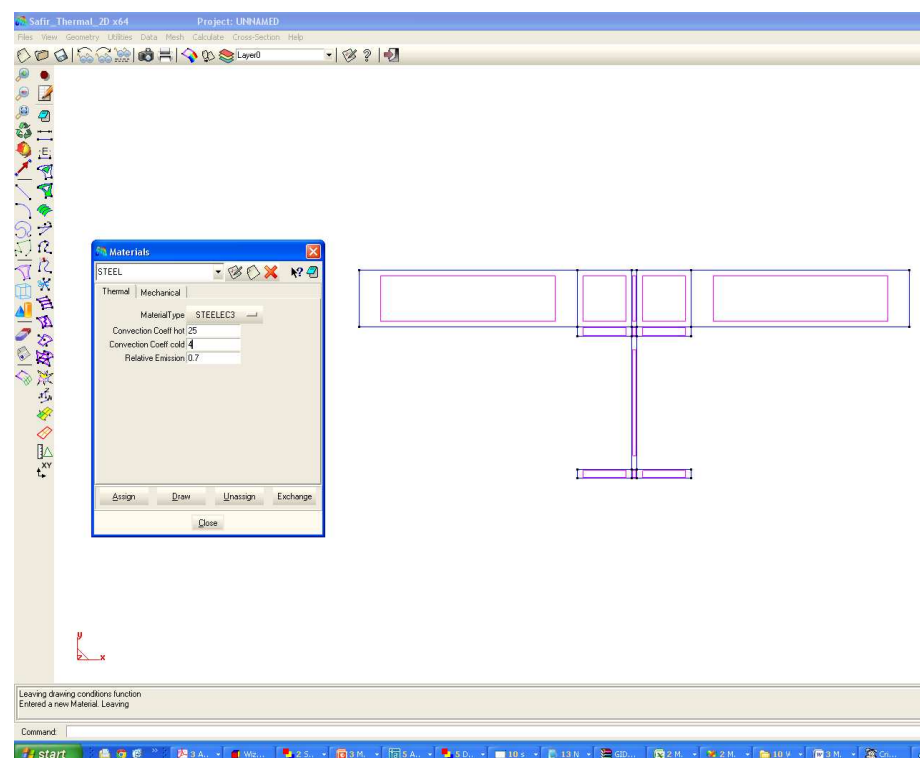
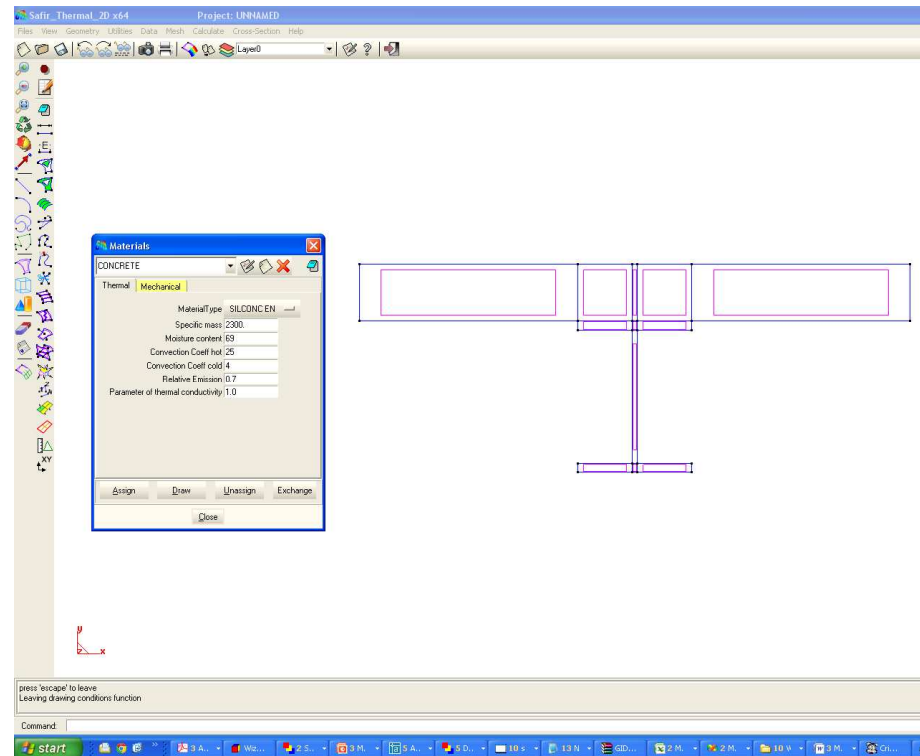
## Assign Frontier condition F20 to the top of the slab



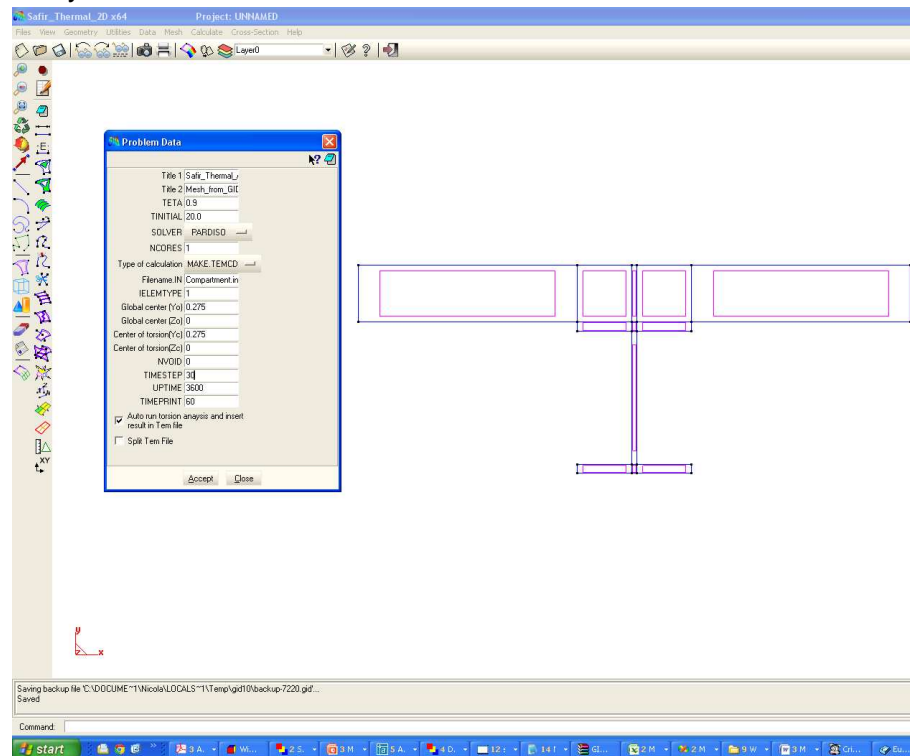
**Assign CFD flux constraints** to the bottom side of the slab and to the beam by writing in the cell "File name of USER-Flux curve" **CFD**.



**Assign material properties.** In order to be consistent with material properties given in the FDS model for the concrete slab, assign the same material with same values.



**Define Problem Data.** Choose MAKE.TEMCD in order to run a thermal analysis that relies on CFD data. Insert the file name of the mechanical input file Compartment.in and make sure that IELEMTYPE corresponds to the right one in the mechanical file (in this example = 1). Move the nodeline of the beam to the slab centerline. Tick Auto run torsion in order to perform torsion analysis as well. **Generate Mesh.**

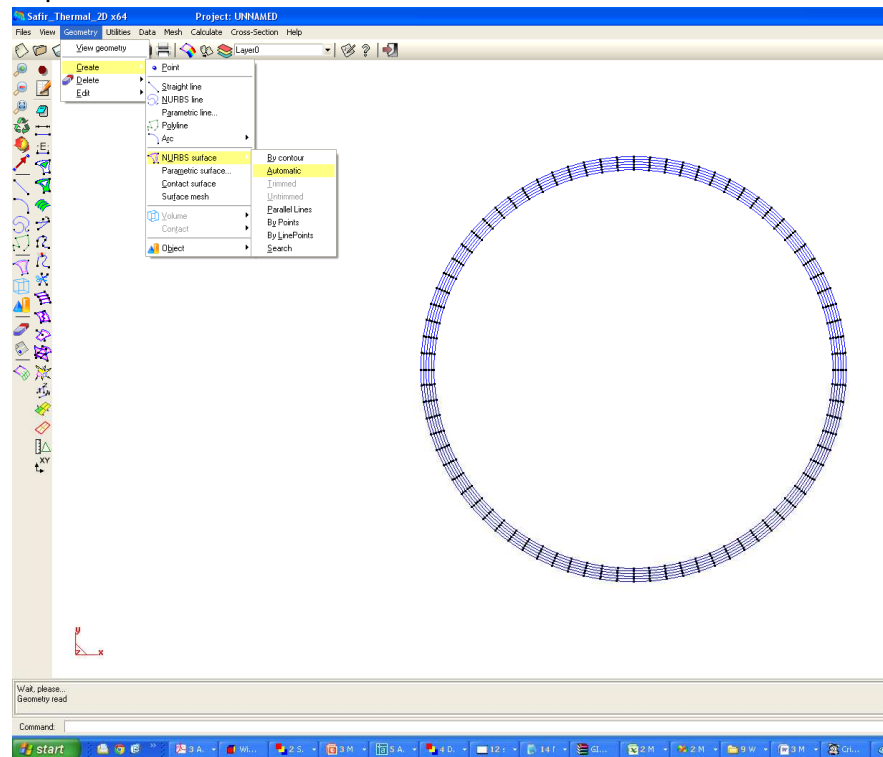


**Generate Mesh.**

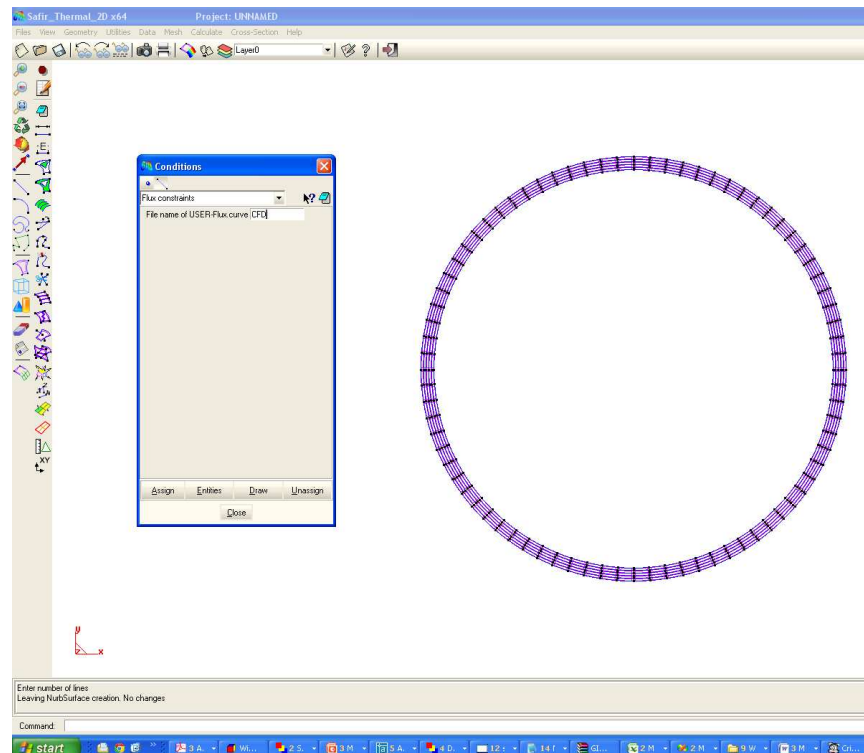
Before running the thermal analysis make sure that the transfer file cfd\_trilin.txt and the mechanical input file Compartment.in be in the same folder of the thermal input file.  
Run the thermal analysis.

## COLUMN TUBE

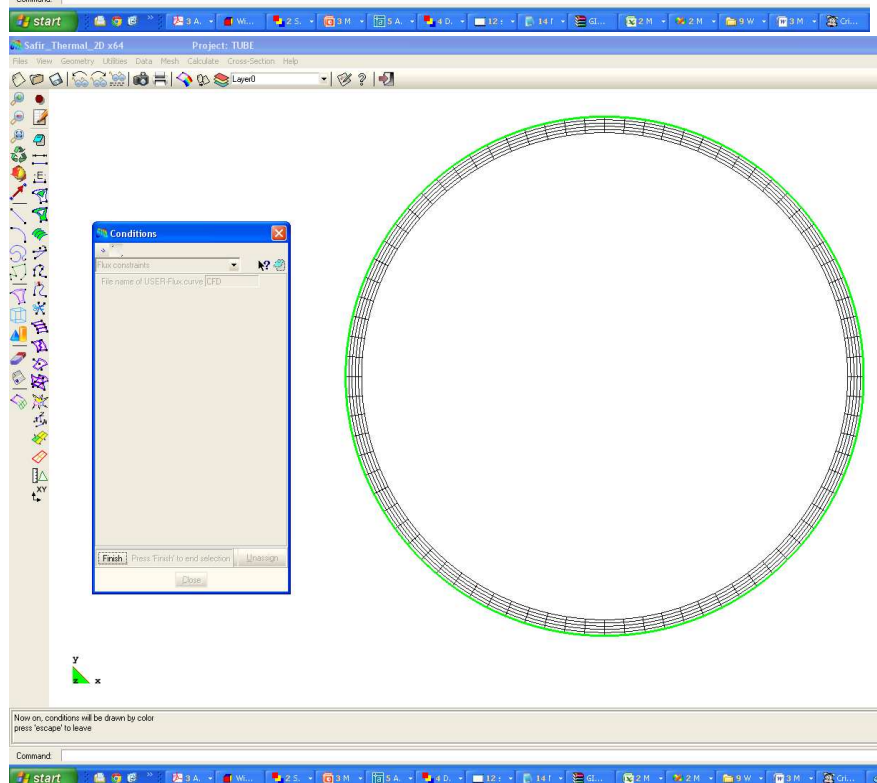
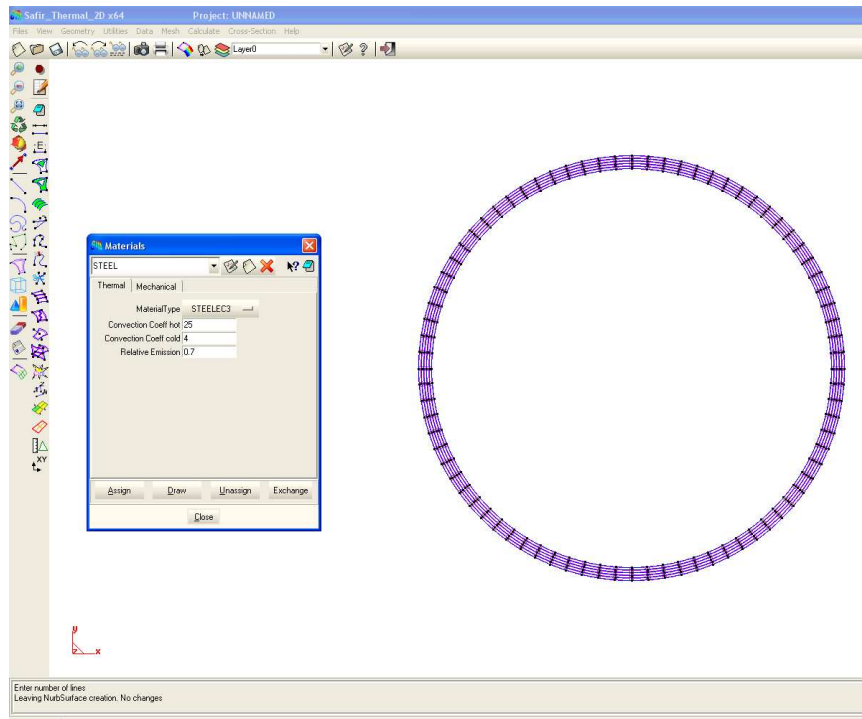
Import the tube.dxf file and create surfaces.



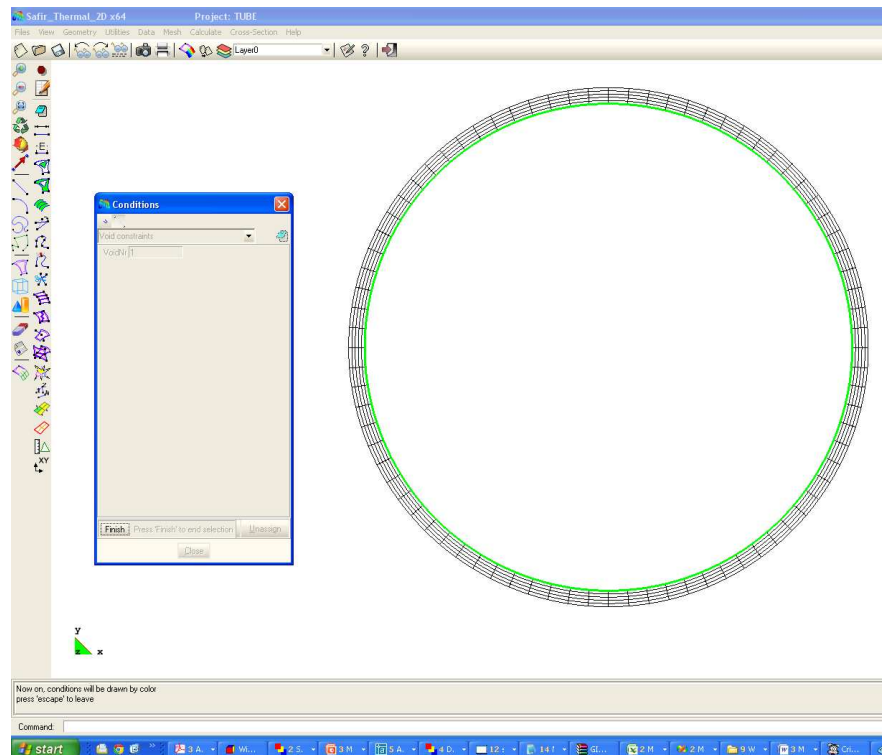
Assign CFD flux constraints to outer side of the tube by writing in the cell "File name of USER-Flux curve" **CFD**.



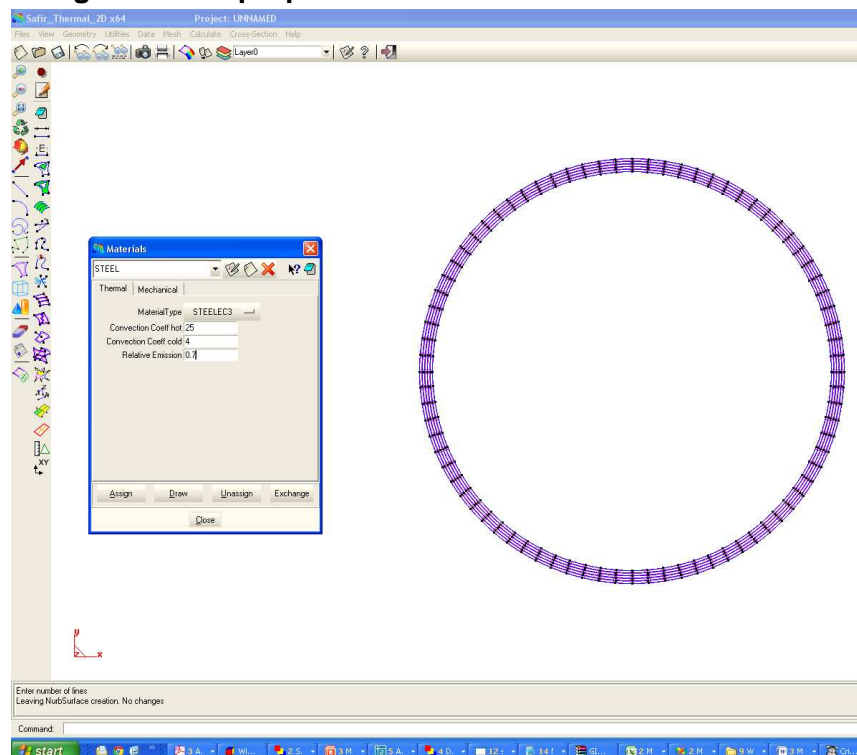




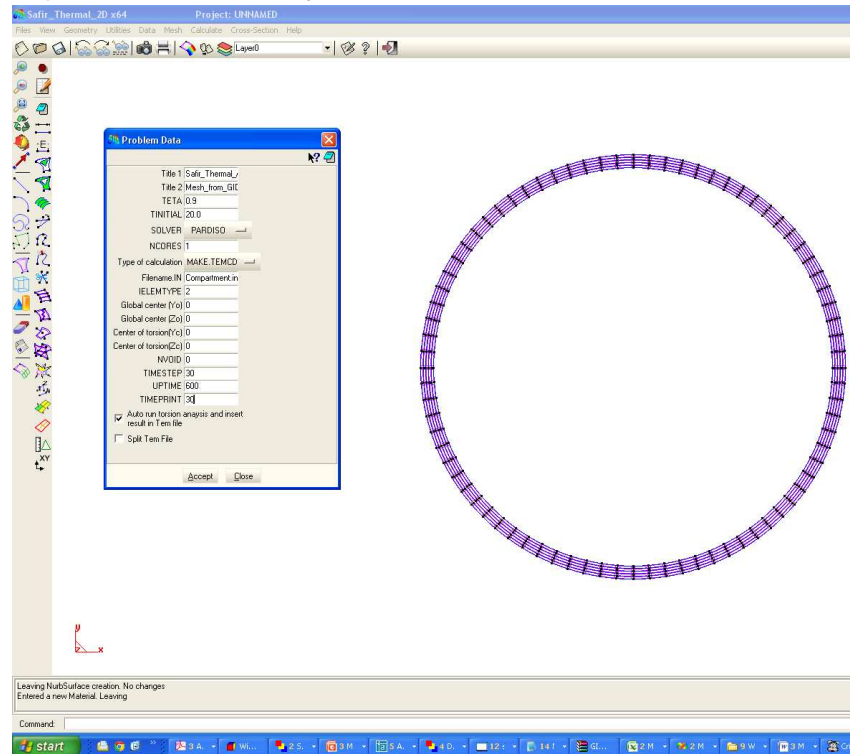
**Assign VOID constraints** to the inner side of the tube by writing in the cell "File name of USER-Flux curve" **CFD**.



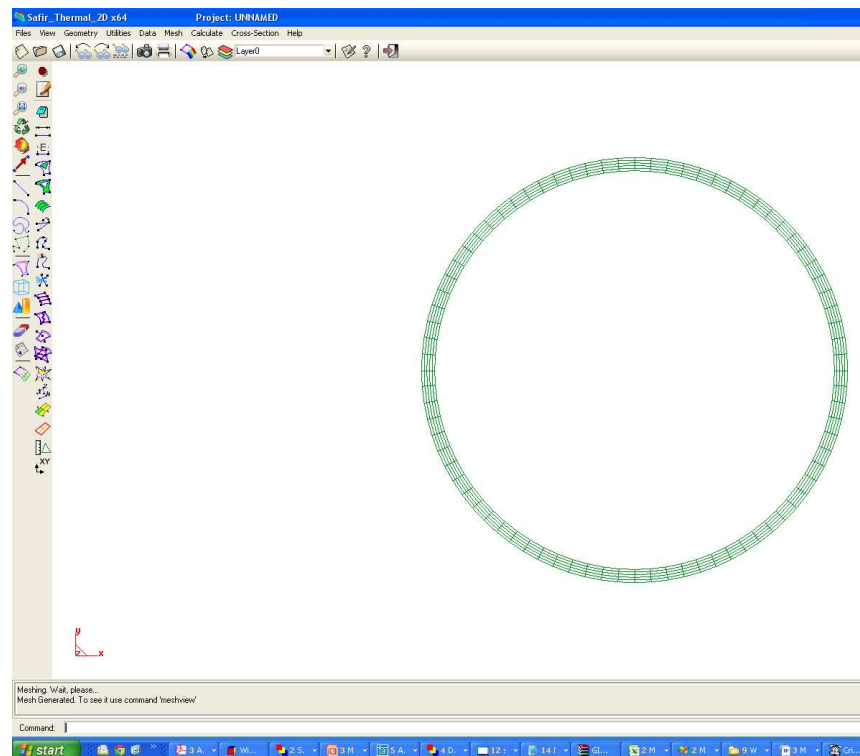
**Assign material properties** of the steel tube.



**Define Problem Data.** Choose MAKE.TEMCD in order to run a thermal analysis with CFD data. Insert the file name of the mechanical input file Compartment.in and make sure that IELEMTYPE corresponds to the right one in the mechanical file (in this example = 2). Tick Auto run torsion in order to perform torsion analysis as well.



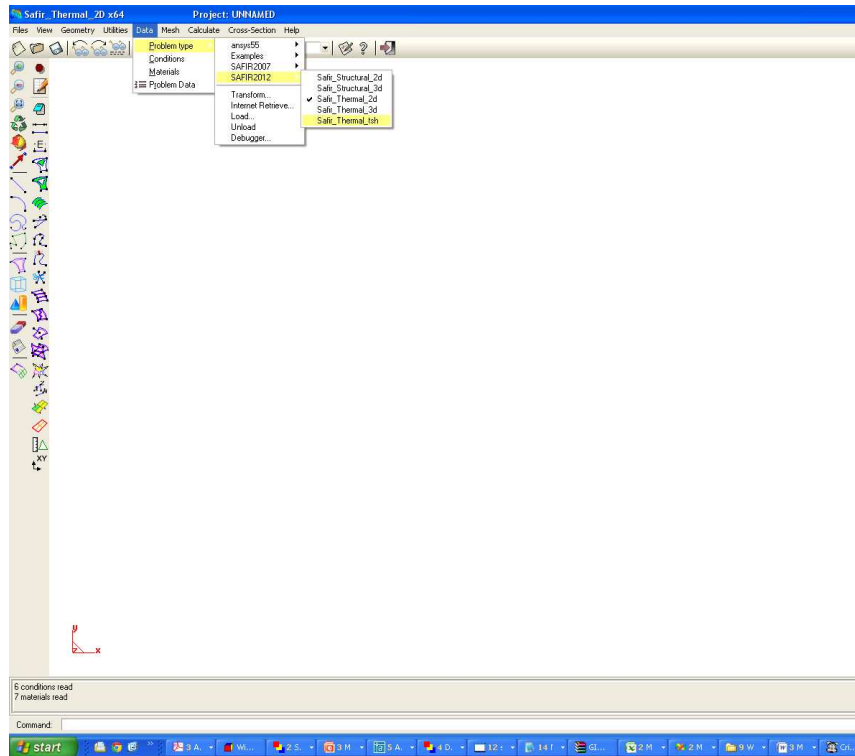
## Generate mesh.



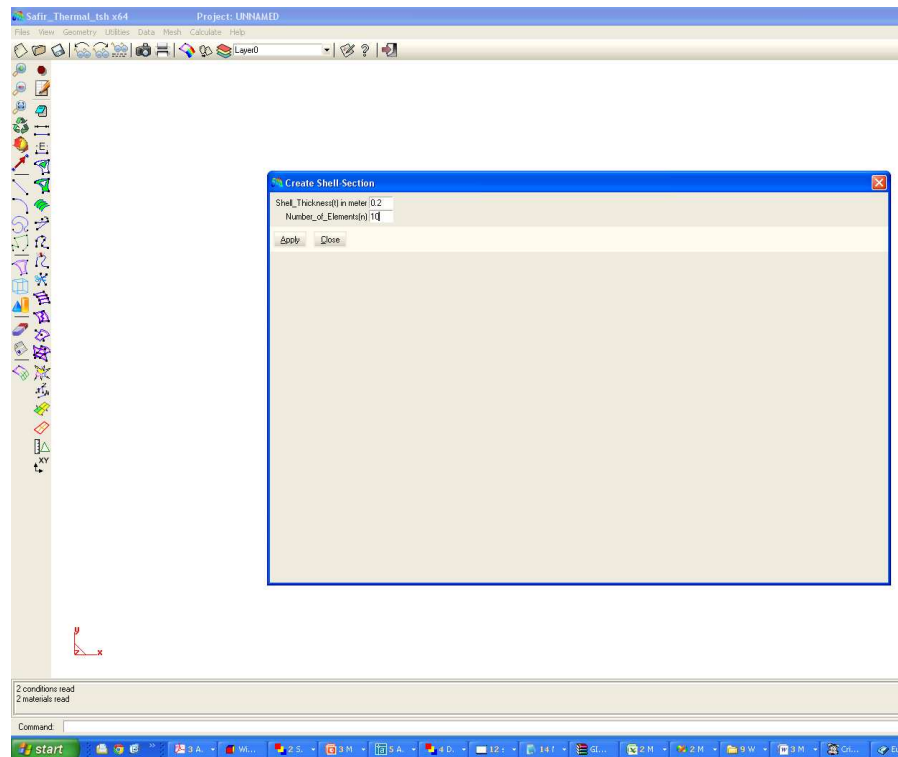
Before running the thermal analysis make sure that the transfer file `cf_d_trilin.txt` and the mechanical input file `Compartment.in` be in the same folder of the thermal input file.  
Run the thermal analysis.

## WALL ELEMENT

Select the **Problem type** -> `Safir_Thermal_tsh` in the new SAFIR 2012 GiD - SAFIR interface.

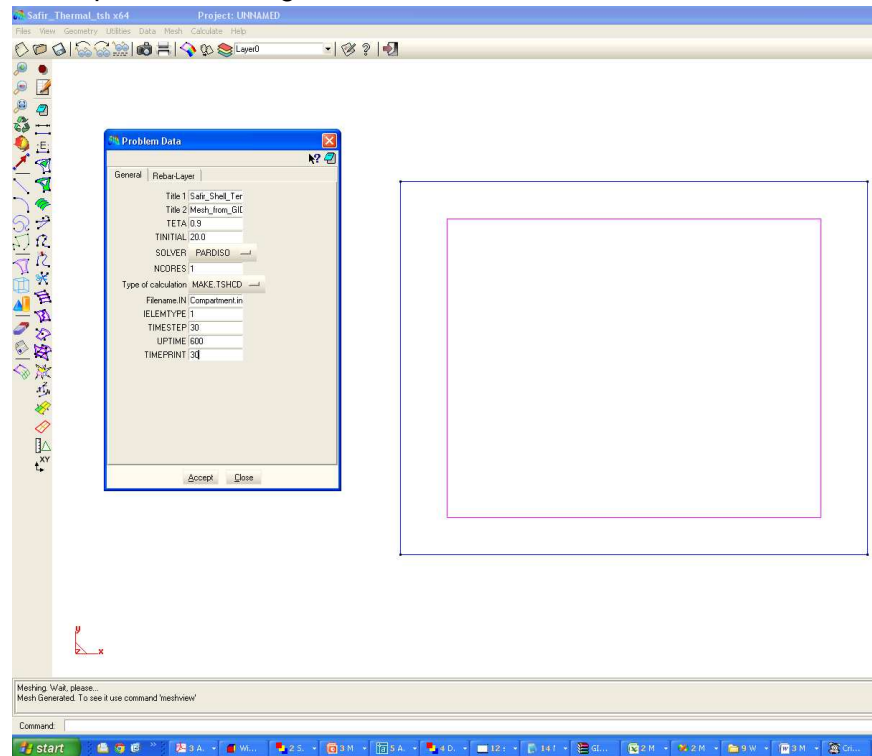


**Insert Thickness (0.2 m) and Number of elements.**

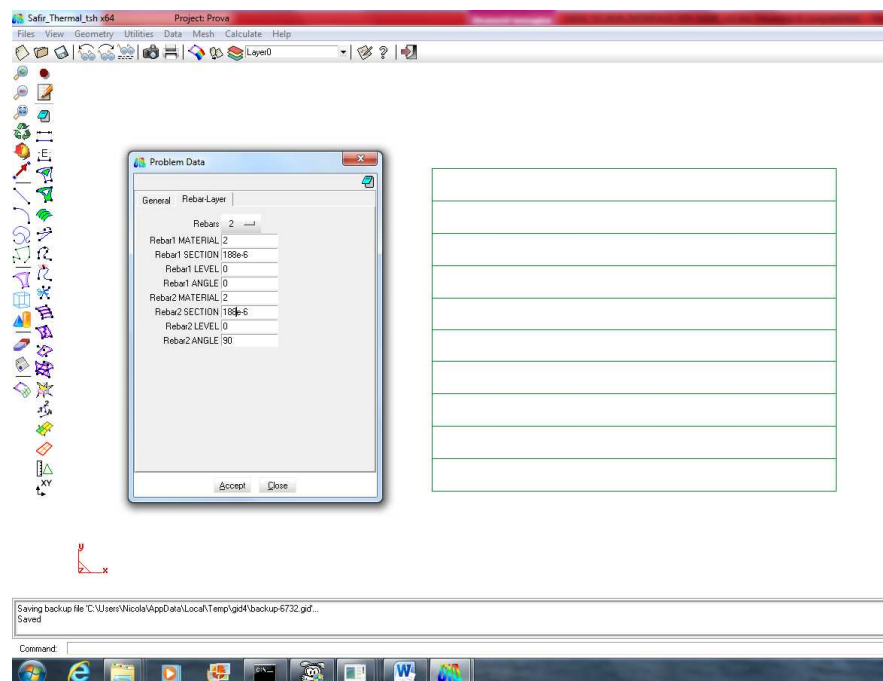


**NOTE:** The same way to assign Boundary **Conditions** (Frontier F20 top and Flux CFD bottom) and **Materials** (same concrete properties) as for the composite beam applies.

**Define Problem Data.** Choose MAKE.TEMSH in order to run a thermal analysis with CFD data. Make sure that IELEMTYPE (in this example = 1) corresponds to the right one in the mechanical file.



**Assign the rebar properties.**



**Before running the thermal analysis make sure that the transfer file cfd\_trilin.txt and the mechanical input file Compartment.in be in the same folder of the thermal input file.**

**Run the thermal analysis.**

**SLAB ELEMENT**

The same way as to create the wall thermal input file but thickness 0.15 m and IELEMENTYPE = 2 in Problem Data.

## 5. PREPARING WHAT NEEDED TO RUN THE MECHANICAL ANALYSIS

In each folder created by GiD for the 4 structural type elements there are the files created by the thermal analyses needed to run the mechanical analysis. These files have .tem extension in the case of beam elements and .tsh in the case of shell elements. They are progressively numbered on the basis of the element number. However, they are not ready to be used yet because in .tem files information about torsion is missing, whilst in .tsh files what is missing is the information about thickness and rebars of the shell.

### BEAM ELEMENT

For beam elements it is necessary to open the .T0R in the relevant folder and copy all lines from **w** to **GJ= value** in the first .tem relative to the beam element type. For, instance for the composite beam:

Open HE400B-1.T0R

Copy all lines from **w** to **GJ= value** in the file **b0001\_1.tem** right before the line where CFD is written. Leave one blank lines before **w** and after **GJ= value**. Save the file.

In an analogously way it is done for the tube column, but the .tem file right now is called **b0007\_1.tem** because the first element of the column tube corresponds to the 7th beam element in the mechanical input file.

```

      w
-0.006088    0.008049    0.681235
-0.004009    0.054313    0.649576
-0.000137    0.066699    0.595848
 0.004201    0.070054    0.539879
 0.008670    0.071006    0.482701
 0.013178    0.071364    0.425265
 0.017715    0.072087    0.367744
 0.022337    0.073486    0.309547
 0.027176    0.082995    0.252360
 0.033910    0.114857    0.174100
 0.010368    0.008003    0.640691
 0.011732    0.035019    0.637178
 0.014328    0.043358    0.592813

.....
.....lines missing.....
.....
 0.020381   -0.068818   -0.121187
 0.031447   -0.133572   -0.009203
 0.029637   -0.132234   -0.022787
 0.027860   -0.130001   -0.036301
 0.026121   -0.126886   -0.049831
 0.024427   -0.122910   -0.063415
 0.022796   -0.118152   -0.077117
 0.021245   -0.112738   -0.090843
 0.019775   -0.106804   -0.104711
 0.018390   -0.100521   -0.118780
 0.017097   -0.094137   -0.133111
```

According to the principle of virtual works,  
GJ= 0.15195E+08



## SHELL ELEMENT

The info regarding the thickness and the rebars of shell elements are included in the 04\_wall-1.dat and 05\_slab-1.dat created during thermal analysis and you can find it in the relevant GiD folders.

The content of the file has to be copied in the first .tsh file created by the thermal analysis (**s0001\_1.tsh** for the wall and **s0019\_1.tsh** for the slab) before the line where CFD is written. Leave one blank line before and after the information of thickness and rebars.

```
THICKNESS    0.2
MATERIAL      1
  REBARS      2
MATERIAL      2
  SECTION     188e-6
  LEVEL       0.0
  ANGLE       0
MATERIAL      2
  SECTION     188e-6
  LEVEL       0.0
  ANGLE       90
```

## 6. HOW TO RUN THE MECHANICAL ANALYSIS

Change the name of the .tem and .tsh in the mechanical input file as follows. They correspond to the first .tem or .tsh of each beam or shell element type.

```
-----
LOCALISED FIRE - MECHANICAL FILE

      NNODE    84
      NDIM     3
      NDDLMAX   7
EVERY_NODE    0
      FROM 1   TO 42 STEP    1 NDDL    6
      FROM 43  TO 49 STEP    1 NDDL    7
      FROM 50  TO 70 STEP    1 NDDL    6
      FROM 71  TO 73 STEP    1 NDDL    7
      FROM 74  TO 82 STEP    1 NDDL    1
      FROM 83  TO 84 STEP    1 NDDL    0
END_NDDL
      STATIC   PURE_NR
      NLOAD    1
      OBLIQUE   0
      COMEBACK 1.0e-5
RENUMGEO 1
      NMAT     4
ELEMENTS
  BEAM      9      2
  NG 2
  NFIBER    414
  SHELL     54      2
  NGTHICK   3
  NGAREA    2
  NREBARS   2
END_ELEM
      NODES
      NODE    1      6.100    0.000    -0.075
      NODE    2      6.100    1.000    -0.075
      NODE    3      6.100    2.000    -0.075
      NODE    4      6.100    3.000    -0.075
      NODE    5      6.100    4.000    -0.075
      NODE    6      6.100    5.000    -0.075
      NODE    7      6.100    6.000    -0.075
      NODE    8      6.100    0.000    1.000
      NODE    9      6.100    1.000    1.000
      NODE   10      6.100    2.000    1.000
      NODE   11      6.100    3.000    1.000
```

NODE	12	6.100	4.000	1.000					
NODE	13	6.100	5.000	1.000					
NODE	14	6.100	6.000	1.000					
NODE	15	6.100	0.000	2.000					
NODE	16	6.100	1.000	2.000					
NODE	17	6.100	2.000	2.000					
NODE	18	6.100	3.000	2.000					
NODE	19	6.100	4.000	2.000					
NODE	20	6.100	5.000	2.000					
NODE	21	6.100	6.000	2.000					
NODE	22	6.100	0.000	3.075					
NODE	23	6.100	1.000	3.075					
NODE	24	6.100	2.000	3.075					
NODE	25	6.100	3.000	3.075					
NODE	26	6.100	4.000	3.075					
NODE	27	6.100	5.000	3.075					
NODE	28	6.100	6.000	3.075					
NODE	29	5.000	0.000	3.075					
NODE	30	5.000	1.000	3.075					
NODE	31	5.000	2.000	3.075					
NODE	32	5.000	3.000	3.075					
NODE	33	5.000	4.000	3.075					
NODE	34	5.000	5.000	3.075					
NODE	35	5.000	6.000	3.075					
NODE	36	4.000	0.000	3.075					
NODE	37	4.000	1.000	3.075					
NODE	38	4.000	2.000	3.075					
NODE	39	4.000	3.000	3.075					
NODE	40	4.000	4.000	3.075					
NODE	41	4.000	5.000	3.075					
NODE	42	4.000	6.000	3.075					
NODE	43	3.000	0.000	3.075					
NODE	44	3.000	1.000	3.075					
NODE	45	3.000	2.000	3.075					
NODE	46	3.000	3.000	3.075					
NODE	47	3.000	4.000	3.075					
NODE	48	3.000	5.000	3.075					
NODE	49	3.000	6.000	3.075					
NODE	50	2.000	0.000	3.075					
NODE	51	2.000	1.000	3.075					
NODE	52	2.000	2.000	3.075					
NODE	53	2.000	3.000	3.075					
NODE	54	2.000	4.000	3.075					
NODE	55	2.000	5.000	3.075					
NODE	56	2.000	6.000	3.075					
NODE	57	1.000	0.000	3.075					
NODE	58	1.000	1.000	3.075					
NODE	59	1.000	2.000	3.075					
NODE	60	1.000	3.000	3.075					
NODE	61	1.000	4.000	3.075					
NODE	62	1.000	5.000	3.075					
NODE	63	1.000	6.000	3.075					
NODE	64	0.000	0.000	3.075					
NODE	65	0.000	1.000	3.075					
NODE	66	0.000	2.000	3.075					
NODE	67	0.000	3.000	3.075					
NODE	68	0.000	4.000	3.075					
NODE	69	0.000	5.000	3.075					
NODE	70	0.000	6.000	3.075					
NODE	71	3.000	3.000	2.000					
NODE	72	3.000	3.000	1.000					
NODE	73	3.000	3.000	-0.075					
NODE	74	3.000	3.000	2.5375					
NODE	75	3.000	3.000	1.500					
NODE	76	3.000	3.000	0.500					
NODE	77	3.000	0.500	3.075					
NODE	78	3.000	1.500	3.075					
NODE	79	3.000	2.500	3.075					
NODE	80	3.000	3.500	3.075					
NODE	81	3.000	4.500	3.075					
NODE	82	3.000	5.500	3.075					
NODE	83	3.000	6.100	4.000					
NODE	84	3.100	3.000	-0.100					
FIXATIONS									
BLOCK	1	F0	F0	F0	NO	NO	NO	NO	
BLOCK	2	F0	NO	F0	NO	NO	NO	NO	

BLOCK	3	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	4	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	5	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	6	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	7	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	64	F0	F0	F0	NO	NO	NO	NO	NO
BLOCK	65	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	66	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	67	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	68	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	69	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	70	F0	NO	F0	NO	NO	NO	NO	NO
BLOCK	73	F0	F0	F0	F0	F0	F0	F0	F0

END\_FIX

NODOFBEAM

**b0001\_1.tem**

TRANSLATE	1	1
TRANSLATE	2	3

END\_TRANS

**b0007\_1.tem**

TRANSLATE	1	1
-----------	---	---

END\_TRANS

ELEM	1	43	77	44	83	1
ELEM	2	44	78	45	83	1
ELEM	3	45	79	46	83	1
ELEM	4	46	80	47	83	1
ELEM	5	47	81	48	83	1
ELEM	6	48	82	49	83	1
ELEM	7	46	74	71	84	2
ELEM	8	71	75	72	84	2
ELEM	9	72	76	73	84	2

NODOF SHELL

**s0001\_1.tsh**

TRANSLATE	1	2
TRANSLATE	2	4

END\_TRANS

**s0019\_1.tsh**

TRANSLATE	1	2
TRANSLATE	2	4

END\_TRANS

ELEM1	1	2	9	8	1	
ELEM	2	2	3	10	9	1
ELEM	3	3	4	11	10	1
ELEM	4	4	5	12	11	1
ELEM	5	5	6	13	12	1
ELEM	6	6	7	14	13	1
ELEM	7	8	9	16	15	1
ELEM	8	9	10	17	16	1
ELEM	9	10	11	18	17	1
ELEM	10	11	12	19	18	1
ELEM	11	12	13	20	19	1
ELEM	12	13	14	21	20	1
ELEM	13	15	16	23	22	1
ELEM	14	16	17	24	23	1
ELEM	15	17	18	25	24	1
ELEM	16	18	19	26	25	1
ELEM	17	19	20	27	26	1
ELEM	18	20	21	28	27	1
ELEM	19	22	23	30	29	2
ELEM	20	23	24	31	30	2
ELEM	21	24	25	32	31	2
ELEM	22	25	26	33	32	2
ELEM	23	26	27	34	33	2
ELEM	24	27	28	35	34	2
ELEM	25	29	30	37	36	2
ELEM	26	30	31	38	37	2
ELEM	27	31	32	39	38	2
ELEM	28	32	33	40	39	2
ELEM	29	33	34	41	40	2
ELEM	30	34	35	42	41	2
ELEM	31	36	37	44	43	2
ELEM	32	37	38	45	44	2
ELEM	33	38	39	46	45	2
ELEM	34	39	40	47	46	2
ELEM	35	40	41	48	47	2
ELEM	36	41	42	49	48	2

```

ELEM      37      43      44      51      50      2
ELEM      38      44      45      52      51      2
ELEM      39      45      46      53      52      2
ELEM      40      46      47      54      53      2
ELEM      41      47      48      55      54      2
ELEM      42      48      49      56      55      2
ELEM      43      50      51      58      57      2
ELEM      44      51      52      59      58      2
ELEM      45      52      53      60      59      2
ELEM      46      53      54      61      60      2
ELEM      47      54      55      62      61      2
ELEM      48      55      56      63      62      2
ELEM      49      57      58      65      64      2
ELEM      50      58      59      66      65      2
ELEM      51      59      60      67      66      2
ELEM      52      60      61      68      67      2
ELEM      53      61      62      69      68      2
ELEM      54      62      63      70      69      2
PRECISION 1.0e-3
LOADS
FUNCTION      FLOAD
DISTRSH      19 0.000000 0.000000 -5310.000000
GDISTRSH     54 0.000000 0.000000 -5310.000000 1
END_LOAD
MATERIALS
STEELEC3EN
2.10e+11 3.00e-01 3.55e+08 1200. 0.
SILCONC2D
3.00e-01 3.00e+07 3.00e+06 0.
INSULATION
STEELEC2
2.06e+11 3.00e-01 5.00e+08 1200. 0.
TIME
1.0 600.0
ENDTIME
EPSTH
IMPRESSION
TIMEPRINT
30.0 600.0
END_TIMEPR
PRINTREACT
PRINTMN

```

**Make sure that all .tem and .tsh files are in the same folder of the mechanical input file.**

**Run the mechanical analysis.**

## Example of transfer file.

```
NSTEPS / Number of time steps N in the CFD analysis
3

TIMES next N lines each contains time value in s
1.00
31.00
61.00

NF (0 implies no such points)
3

XYZ_FLUXES
0.500 0.500 0.500
0.500 1.500 0.500
0.500 2.500 0.500

NN
2

XYZ_NORMALS
-1 1 0 0 0 0

NP
27

XYZ_INTENSITIES
0.500 0.500 0.500
1.500 0.500 0.500
2.500 0.500 0.500
0.500 1.500 0.500
1.500 1.500 0.500
2.500 1.500 0.500
0.500 2.500 0.500
1.500 2.500 0.500
2.500 2.500 0.500
0.500 0.500 1.500
1.500 0.500 1.500
2.500 0.500 1.500
0.500 1.500 1.500
1.500 1.500 1.500
2.500 1.500 1.500
0.500 2.500 1.500
1.500 2.500 1.500
2.500 2.500 1.500
0.500 0.500 2.500
1.500 0.500 2.500
2.500 0.500 2.500
0.500 1.500 2.500
1.500 1.500 2.500
2.500 1.500 2.500
0.500 2.500 2.500
1.500 2.500 2.500
2.500 2.500 2.500

NI
8

XYZ_DIRECTIONS
0.500 0.500 0.707
-0.500 0.500 0.707
-0.500 -0.500 0.707
0.500 -0.500 0.707
0.500 0.500 -0.707
-0.500 0.500 -0.707
-0.500 -0.500 -0.707
0.500 -0.500 -0.707

TIME \time in s (real)
1.00

FLUXES
308.48 0.93 18504.20 418.74
308.48 1.18 21134.32 418.74
308.48 1.09 18504.20 418.74

INTENSITIES
308.48 0.93 3585.63 133.29 133.29 5242.76 5242.76 133.29 133.29 9489.14
294.88 1.26 823.76 133.29 133.29 1755.89 1755.89 133.29 133.29 6236.26
294.88 0.78 271.38 133.29 133.29 633.88 633.88 133.29 133.29 3585.63
308.48 1.18 4966.57 133.29 133.29 4966.57 8487.96 133.29 133.29 8487.96
294.88 1.02 1514.23 133.29 133.29 1514.23 4609.83 133.29 133.29 4609.83
294.88 0.77 513.05 133.29 133.29 513.05 2260.32 133.29 133.29 2260.32
308.48 1.09 5242.76 133.29 133.29 3585.63 9489.14 133.29 133.29 5242.76
294.88 0.86 1755.89 133.29 133.29 823.76 6236.26 133.29 133.29 1755.89
294.88 0.41 633.88 133.29 133.29 271.38 3585.63 133.29 133.29 633.88
308.48 1.33 4966.57 133.29 133.29 8487.96 4966.57 133.29 133.29 8487.96
```

294.88	1.22	1514.23	133.29	133.29	4609.83	1514.23	133.29	133.29	4609.83
294.88	0.85	513.05	133.29	133.29	2260.32	513.05	133.29	133.29	2260.32
308.48	0.84	7728.44	133.29	133.29	7728.44	7728.44	133.29	133.29	7728.44
294.88	0.93	3585.63	133.29	133.29	3585.63	3585.63	133.29	133.29	3585.63
294.88	0.79	1537.24	133.29	133.29	1537.24	1537.24	133.29	133.29	1537.24
308.48	0.93	8487.96	133.29	133.29	4966.57	8487.96	133.29	133.29	4966.57
294.88	1.08	4609.83	133.29	133.29	1514.23	4609.83	133.29	133.29	1514.23
294.88	0.89	2260.32	133.29	133.29	513.05	2260.32	133.29	133.29	513.05
308.48	0.82	5242.76	133.29	133.29	9489.14	3585.63	133.29	133.29	5242.76
294.88	0.91	1755.89	133.29	133.29	6236.26	823.76	133.29	133.29	1755.89
294.88	0.82	633.88	133.29	133.29	3585.63	271.38	133.29	133.29	633.88
308.48	1.41	8487.96	133.29	133.29	8487.96	4966.57	133.29	133.29	4966.57
294.88	1.20	4609.83	133.29	133.29	4609.83	1514.23	133.29	133.29	1514.23
294.88	0.38	2260.32	133.29	133.29	2260.32	513.05	133.29	133.29	513.05
308.48	0.77	9489.14	133.29	133.29	5242.76	5242.76	133.29	133.29	3585.63
294.88	0.40	6236.26	133.29	133.29	1755.89	1755.89	133.29	133.29	823.76
294.88	0.00	3585.63	133.29	133.29	633.88	633.88	133.29	133.29	271.38

TIME \time in s (real)  
31.00

FLUXES

346.75	4.82	18504.20	418.74
346.92	4.84	21134.32	418.74
346.75	4.82	18504.20	418.74

INTENSITIES

346.75	4.82	3585.63	133.29	133.29	5242.76	5242.76	133.29	133.29	9489.14
337.38	3.77	823.76	133.29	133.29	1755.89	1755.89	133.29	133.29	6236.26
341.85	3.28	271.38	133.29	133.29	633.88	633.88	133.29	133.29	3585.63
346.92	4.84	4966.57	133.29	133.29	4966.57	8487.96	133.29	133.29	8487.96
337.03	3.66	1514.23	133.29	133.29	1514.23	4609.83	133.29	133.29	4609.83
341.44	2.69	513.05	133.29	133.29	513.05	2260.32	133.29	133.29	2260.32
346.75	4.82	5242.76	133.29	133.29	3585.63	9489.14	133.29	133.29	5242.76
337.38	3.77	1755.89	133.29	133.29	823.76	6236.26	133.29	133.29	1755.89
341.84	3.27	633.88	133.29	133.29	271.38	3585.63	133.29	133.29	633.88
355.44	4.35	4966.57	133.29	133.29	8487.96	4966.57	133.29	133.29	8487.96
350.43	3.45	1514.23	133.29	133.29	4609.83	1514.23	133.29	133.29	4609.83
351.96	4.41	513.05	133.29	133.29	2260.32	513.05	133.29	133.29	2260.32
356.05	4.54	7728.44	133.29	133.29	7728.44	7728.44	133.29	133.29	7728.44
350.35	3.71	3585.63	133.29	133.29	3585.63	3585.63	133.29	133.29	3585.63
352.41	4.25	1537.24	133.29	133.29	1537.24	1537.24	133.29	133.29	1537.24
355.44	4.35	8487.96	133.29	133.29	4966.57	8487.96	133.29	133.29	4966.57
350.43	3.45	4609.83	133.29	133.29	1514.23	4609.83	133.29	133.29	1514.23
351.95	4.41	2260.32	133.29	133.29	513.05	2260.32	133.29	133.29	513.05
365.42	4.35	5242.76	133.29	133.29	9489.14	3585.63	133.29	133.29	5242.76
358.98	4.33	1755.89	133.29	133.29	6236.26	823.76	133.29	133.29	1755.89
353.31	0.82	633.88	133.29	133.29	3585.63	271.38	133.29	133.29	633.88
366.14	4.27	8487.96	133.29	133.29	8487.96	4966.57	133.29	133.29	4966.57
359.85	4.25	4609.83	133.29	133.29	4609.83	1514.23	133.29	133.29	1514.23
354.15	0.82	2260.32	133.29	133.29	2260.32	513.05	133.29	133.29	513.05
365.43	4.35	9489.14	133.29	133.29	5242.76	5242.76	133.29	133.29	3585.63
358.98	4.33	6236.26	133.29	133.29	1755.89	1755.89	133.29	133.29	823.76
353.30	0.00	3585.63	133.29	133.29	633.88	633.88	133.29	133.29	271.38

TIME \time in s (real)  
61.00

FLUXES

379.48	4.88	18504.20	418.74
380.13	4.89	21134.32	418.74
379.48	4.88	18504.20	418.74

INTENSITIES

379.48	4.88	3585.63	133.29	133.29	5242.76	5242.76	133.29	133.29	9489.14
371.72	3.81	823.76	133.29	133.29	1755.89	1755.89	133.29	133.29	6236.26
375.89	3.74	271.38	133.29	133.29	633.88	633.88	133.29	133.29	3585.63
380.13	4.89	4966.57	133.29	133.29	4966.57	8487.96	133.29	133.29	8487.96
371.35	3.71	1514.23	133.29	133.29	1514.23	4609.83	133.29	133.29	4609.83
376.02	2.94	513.05	133.29	133.29	513.05	2260.32	133.29	133.29	2260.32
379.48	4.88	5242.76	133.29	133.29	3585.63	9489.14	133.29	133.29	5242.76
371.72	3.81	1755.89	133.29	133.29	823.76	6236.26	133.29	133.29	1755.89
375.89	3.72	633.88	133.29	133.29	271.38	3585.63	133.29	133.29	633.88
389.03	4.27	4966.57	133.29	133.29	8487.96	4966.57	133.29	133.29	8487.96
384.12	3.09	1514.23	133.29	133.29	4609.83	1514.23	133.29	133.29	4609.83
385.83	4.47	513.05	133.29	133.29	2260.32	513.05	133.29	133.29	2260.32
390.04	4.58	7728.44	133.29	133.29	7728.44	7728.44	133.29	133.29	7728.44
384.10	3.64	3585.63	133.29	133.29	3585.63	3585.63	133.29	133.29	3585.63
386.91	4.33	1537.24	133.29	133.29	1537.24	1537.24	133.29	133.29	1537.24
389.03	4.26	8487.96	133.29	133.29	4966.57	8487.96	133.29	133.29	4966.57
384.12	3.09	4609.83	133.29	133.29	1514.23	4609.83	133.29	133.29	1514.23
385.83	4.47	2260.32	133.29	133.29	513.05	2260.32	133.29	133.29	513.05
398.45	4.35	5242.76	133.29	133.29	9489.14	3585.63	133.29	133.29	5242.76
392.91	4.43	1755.89	133.29	133.29	6236.26	823.76	133.29	133.29	1755.89
387.73	0.50	633.88	133.29	133.29	3585.63	271.38	133.29	133.29	633.88
399.49	4.20	8487.96	133.29	133.29	8487.96	4966.57	133.29	133.29	4966.57
394.44	4.26	4609.83	133.29	133.29	4609.83	1514.23	133.29	133.29	1514.23
388.98	0.50	2260.32	133.29	133.29	2260.32	513.05	133.29	133.29	513.05
398.45	4.34	9489.14	133.29	133.29	5242.76	5242.76	133.29	133.29	3585.63

392.91	4.43	6236.26	133.29	133.29	1755.89	1755.89	133.29	133.29	823.76
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